



	<h1>2019</h1> <p><b>INSPECTION AND MECHANICAL INTEGRITY SUMMIT</b></p>	<p>JANUARY 28-31 GALVESTON ISLAND TEXAS   USA</p> <hr/> <p>Brought to you by <i>energy</i> <b>API</b>   AMERICAN PETROLEUM INSTITUTE</p>
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**Vibration integrity management**  
New tools to avoid fatigue failure

# Speaker

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Service Lead Americas –

Static Equipment and Structures, Wood

- 16 years' industry experience
- Field of expertise: vibration engineering



# Agenda

1. Introduction
2. Conclusions from 2017 Presentation
3. Complementary approach to RBI (API 570)
4. Excitation mechanisms
5. How companies can assess vibration risks
6. Recommendations
7. Conclusion



# Introduction

- Vibration-related fatigue failure on piping is a real threat to facilities
- Vibration should be included in integrity programs
- How can owners/operators be proactive to understand this risk?
- How can owners/operators take corrective action before the failure and loss of containment occurs?





# Conclusions (from 2017)

- Vibration is a **significant threat** to facility integrity
- Vibration is **not managed effectively** in most integrity programs
- **Tools and experience exist** to assist integrity professionals
- Vibration **screening is complementary** to integrity methods
- **Field vibration measurement is effective** alongside NDT

**A successful integrity program  
includes vibration considerations**

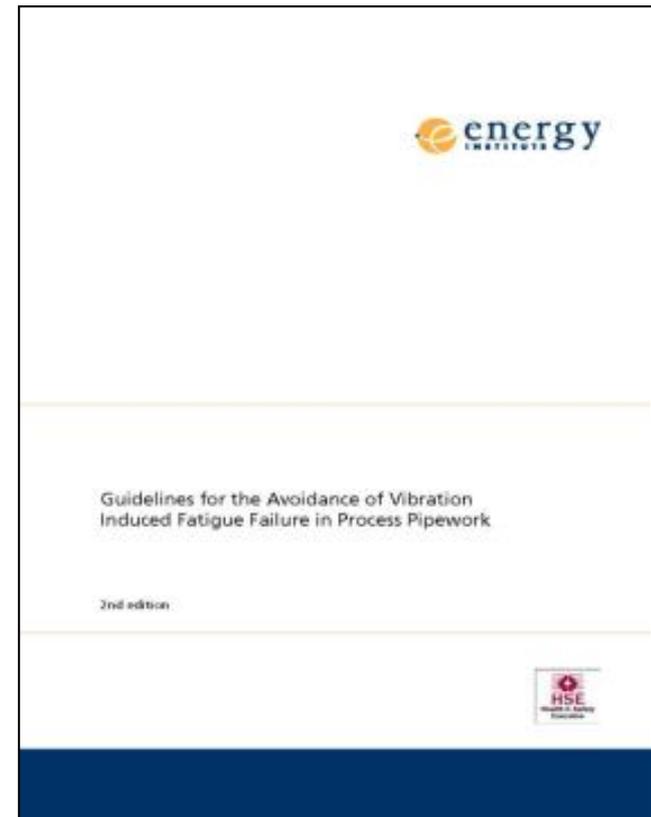


# Avoid surprises!



# Energy Institute

Guidelines for the **Avoidance of  
Vibration Induced Fatigue Failure**  
in Process Pipework  
2nd Ed., 2008 (EI **AVIFF**)



# Complementary approach to API 570

## Piping mechanical integrity (per API 570)

## Vibration assessment (per EI guidelines)

### What's in scope?

Consequence and criticality assessment determines priority lines to focus on (safety and production critical)

Typically includes a mainline assessment (primary process piping) and rotating equipment

### What could go wrong?

Markup PFDs / P&IDs (circuitization)  
Identify likely damage mechanisms

Small-bore connections, reciprocating equipment, turbulence, flare lines, valves, resonance

### How bad is it?

Assess process and materials to determine corrosion and environmental cracking threats

Assess vibration mechanisms using appropriate screening tools

### How can we manage it?

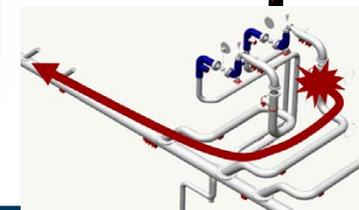
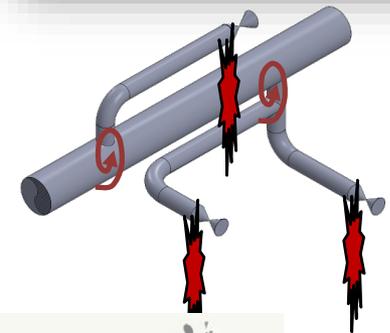
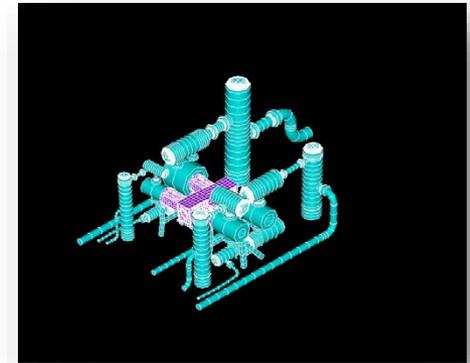
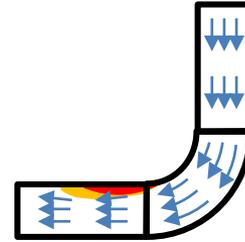
- Develop inspection test plans (ITPs)
- Process/materials recommendations
- Establish integrity operating windows (IOWs)

- Inspection locations included in ITP
- Engineered solutions (clamps, braces, etc)
  - IOWs (flow limits, equipment speed range)
  - Manage anomalies until close-out



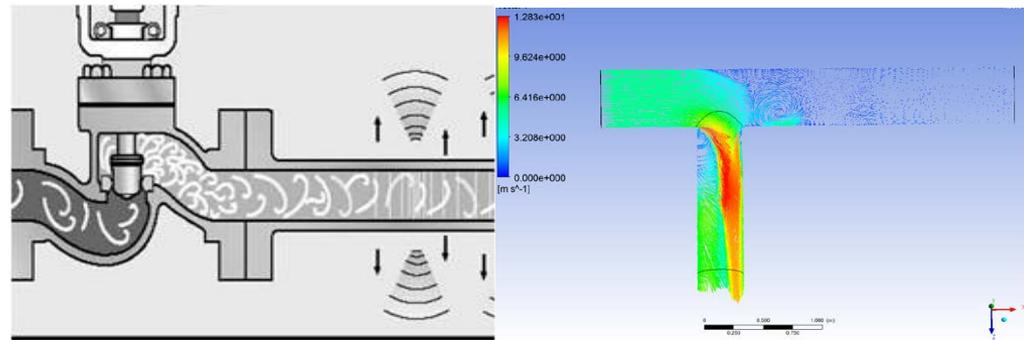
# Excitation mechanisms from EI AVIFF

- Flow-induced turbulence
- Mechanical excitation and pulsation
- Pulsation: rotating stall
- Pulsation: flow-induced excitation
- High-frequency acoustic excitation
- Surge: momentum changes due to valve operation
- Cavitation and flashing



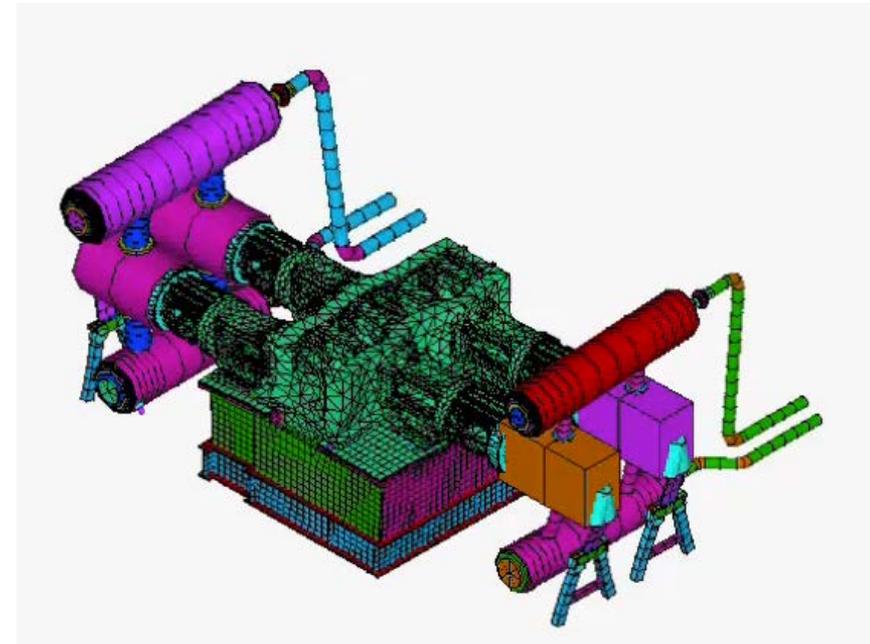
# Flow-induced turbulence (FIT)

- Dominant source for FIV turbulence is generated at flow discontinuities in the system, such as:
  - Process equipment
  - Partially closed valves
  - Short radius or mitred bends
  - Tees and reducers
- Turbulence is generated in fluid flowing in piping, leading to vibration with frequency ranges up to 200 Hz



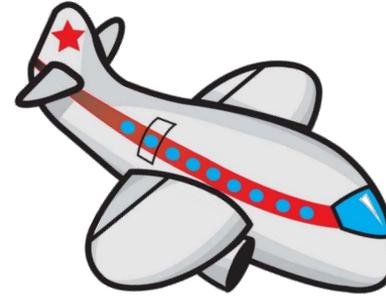
# Mechanical excitation and pulsation

- Reciprocating and positive displacement machines
- Energy at orders of operating speed
- Mechanical excitation close to compressors
- Uncontrolled pulsations travel upstream and downstream, impact piping



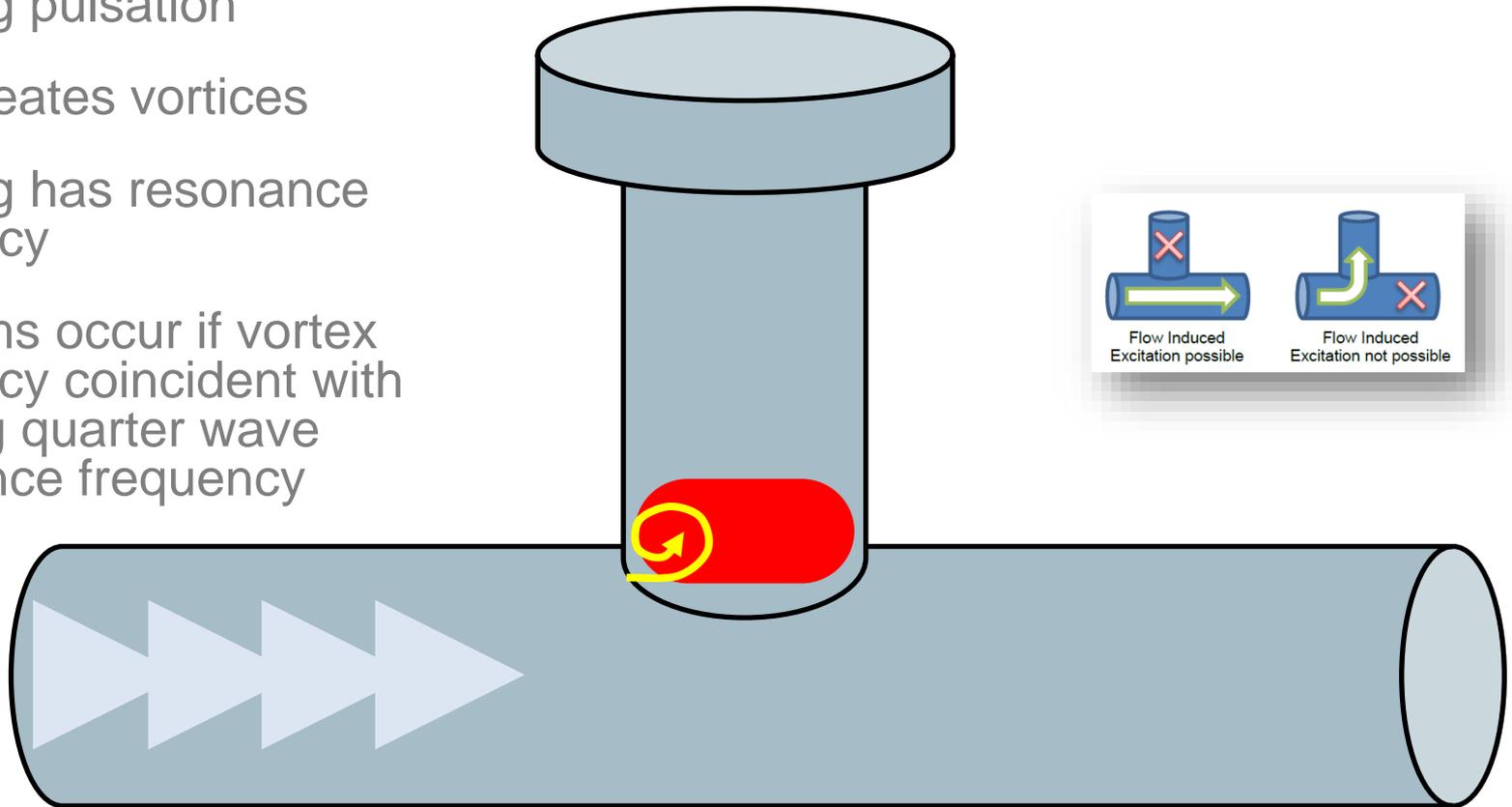
# Pulsation: rotating stall

Creates sub-synchronous pulsations



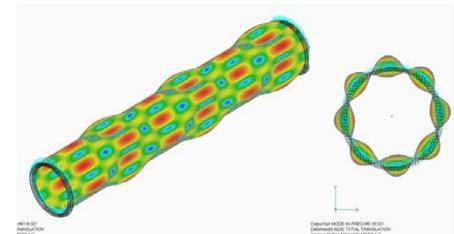
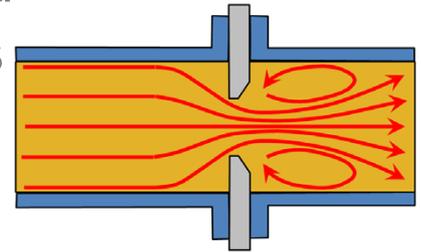
# Pulsation: flow-induced excitation

- Deadleg pulsation
- Flow creates vortices
- Deadleg has resonance frequency
- Problems occur if vortex frequency coincident with deadleg quarter wave resonance frequency



# High-frequency acoustic excitation (AIV)

- High levels of acoustic energy can be generated in high-capacity gas-pressure-reducing systems such as:
  - Pressure relief
  - Blow down
  - Flow or pressure control
- High levels of acoustic energy can **result in severe piping vibration**, leading to piping component fatigue failure in as little as a few hours
  - Typical frequency range: 300 Hz to 4000 Hz

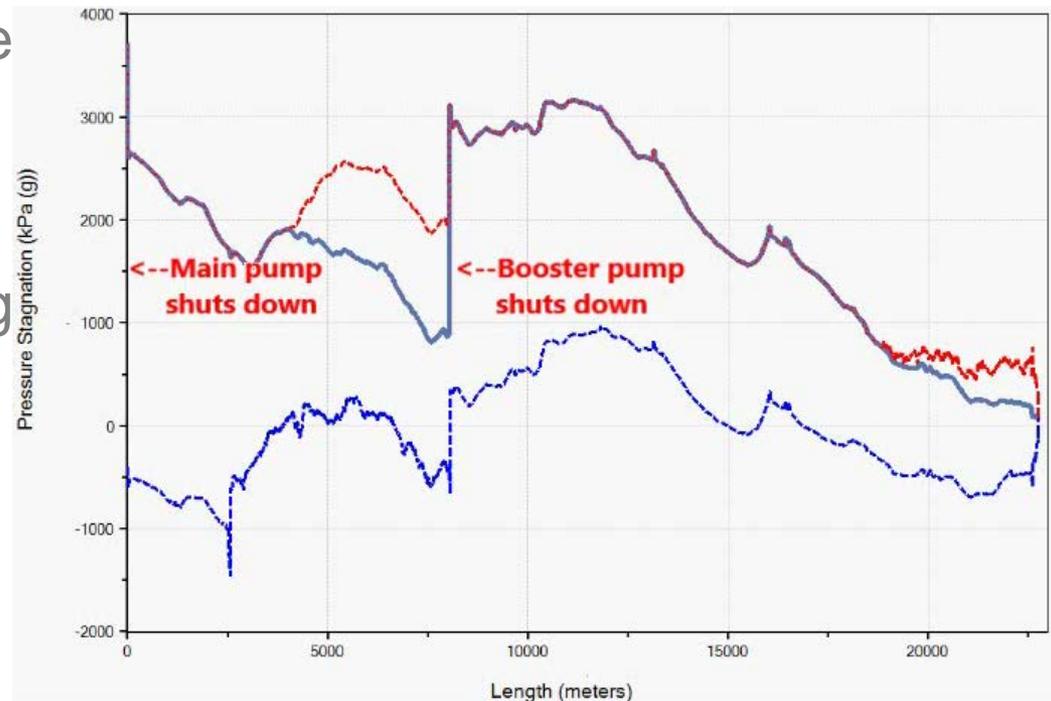


# High-frequency acoustic excitation (AIV)



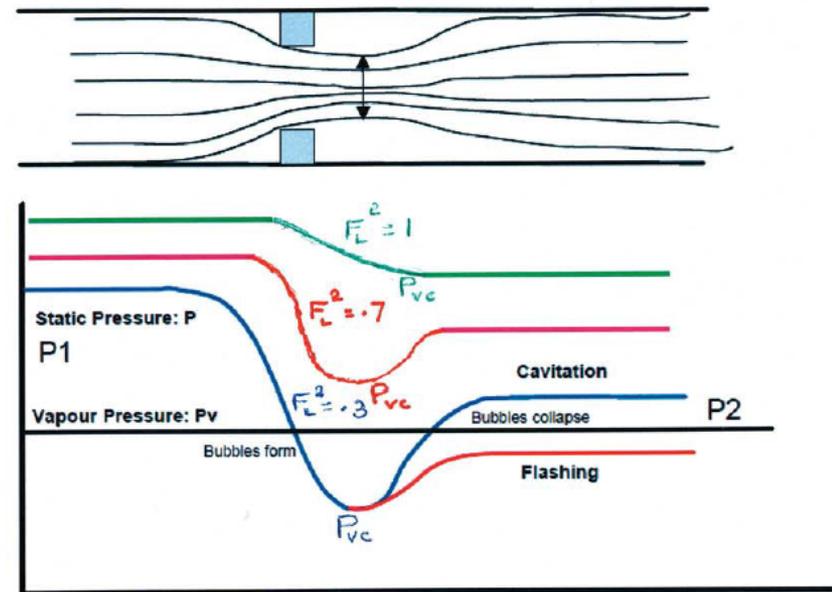
# Surge: momentum changes due to valve operation

- Localized changes in the fluid velocity
  - Valve closing
  - Pump start and stop
- Pressure peaks traveling through the pipe
  - Excitation of localized pipe resonance
  - Trip relief valve



# Cavitation and flashing

- When local pressure in liquid goes below vapor pressure
- Occurs near pressure-reducing areas like pump inlets, valves, orifice plates
- Cavitation is when the bubbles quickly collapse
- Flashing is when the bubbles remain in the liquid



# How you do know when to be worried?



# Know where to focus your efforts



# Vibration screening tool Veridian

wood Veridian  
Web tools for vibration, dynamics and noise

Current project  
CA00703 - Modoc In

System 2/System 2 - Electrostatic Treatment\_R00

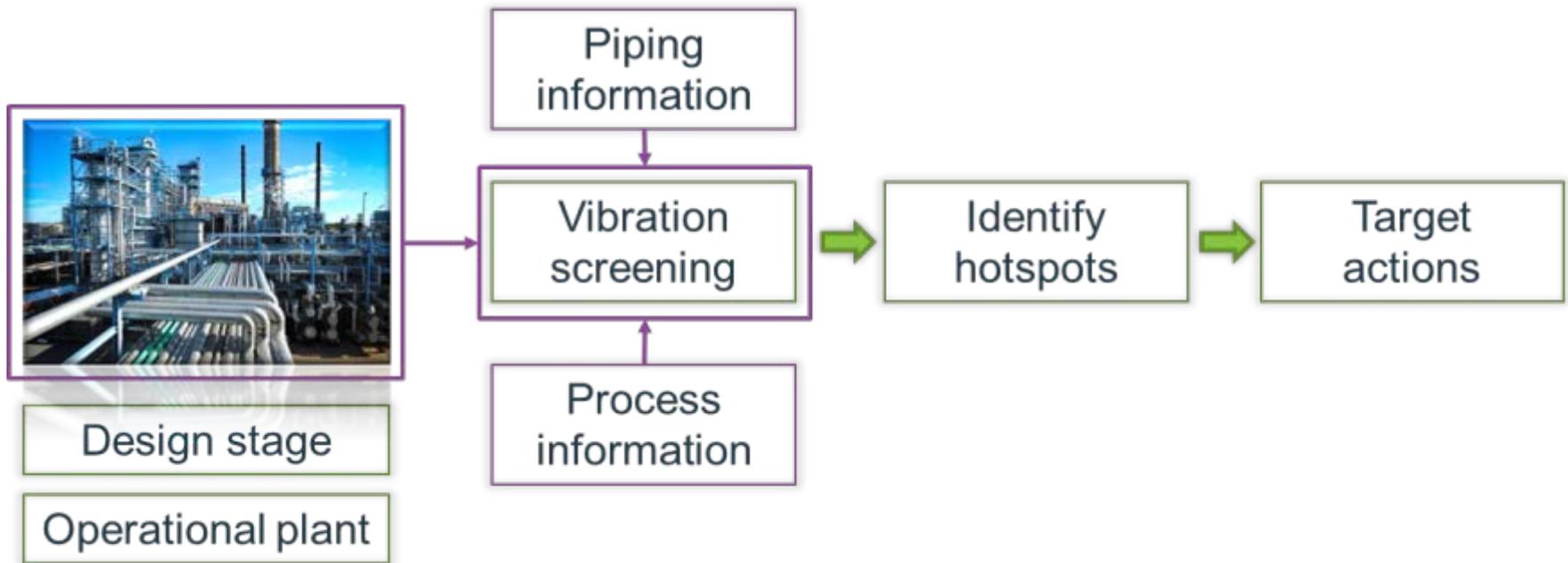
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Record ID	P&ID	Line reference	Description	Notes	Pipe details	Stream	% of stream	Qualitative assessment (modules)	Flow-induced turbulence	Valve transients	Cavitation and flashing	Small bore connections
1	0381-MI20-90DP-3190	14"-PL-A5D-19023-2H1	1st Stg Electrostatic		14" CBI-A5D 10S Stainless Steel	Stream 1009 (Max Oil) (liquid)	50	v=2.2 m/s pv=3,562	0.15			
2	0381-MI20-90DP-3190	14"-PL-A5D-19023-2H1	1st Stg Electrostatic		14" CBI-A5D 10S Stainless Steel	Stream 1009 (Max Oil) (liquid)	50	v=2.2 m/s pv=3,562	0.15			
3	0381-MI20-90DP-3190	14"-PL-A5D-19023-2H1	1st Stg Electrostatic		14" CBI-A5D 10S Stainless Steel	Stream 1009 (Max Oil) (liquid)	100	v=4.3 m/s pv=14,648	1.38	0.10	0.00	0.74
4	0381-MI20-90DP-3190	14"-A5D-2RNX-19063	1st Stg Electrostatic		14" CBI-A5D 10S Stainless Steel	Stream 1010 (Max Oil) (liquid)	100	v=3.2 m/s pv=20,085	0.77	0.60	1.00	0.66
5	0381-MI20-90DP-3190	14"-A5D-2RNX-19064	1st Stg Electrostatic		14" CBI-A5D 10S Stainless Steel	Stream 1011 (Max Oil) (multiphase)	100	v=7.9 m/s pv=20,085	0.83	0.47	1.00	0.68
6	0381-MI20-90DP-3190	16"-PL-A5D-19024-2H1	1st Stg Electrostatic		16" CBI-A5D 10S Stainless Steel	Stream 1012 (Max Oil) (multiphase)	100	v=6.1 m/s pv=12,098	0.49	0.14	1.00	0.70
7	0381-MI20-90DP-3192	16"-A5D-2RNX-19233	1st Stg Electrostatic		16" CBI-A5D 10S Stainless Steel	Stream 1013 (Max Oil) (multiphase)	100	v=14.3 m/s pv=26,322	1.14			0.64
8	0381-MI20-90DP-3190	None	1st Stg Electrostatic		18" CBI-A5D 10S Stainless Steel	Stream 1013 (Max Oil) (multiphase)	100	v=11.2 m/s pv=17,493	0.68			
9	0381-MI20-90DP-3190	None	1st Stg Electrostatic		6" CBI-A5D 10S Stainless Steel	Stream 4502 (Max Oil) (liquid)	100	v=0.4 m/s pv=121	0.01			
10	0381-MI20-90DP-3190	3"-A5D-5RSX-19069	1st Stg Electrostatic		3" CBI-A5D 10S Stainless Steel	Stream 4502 (Max Oil) (liquid)	100	v=1.3 m/s pv=1,748	0.08	1.00	0.00	

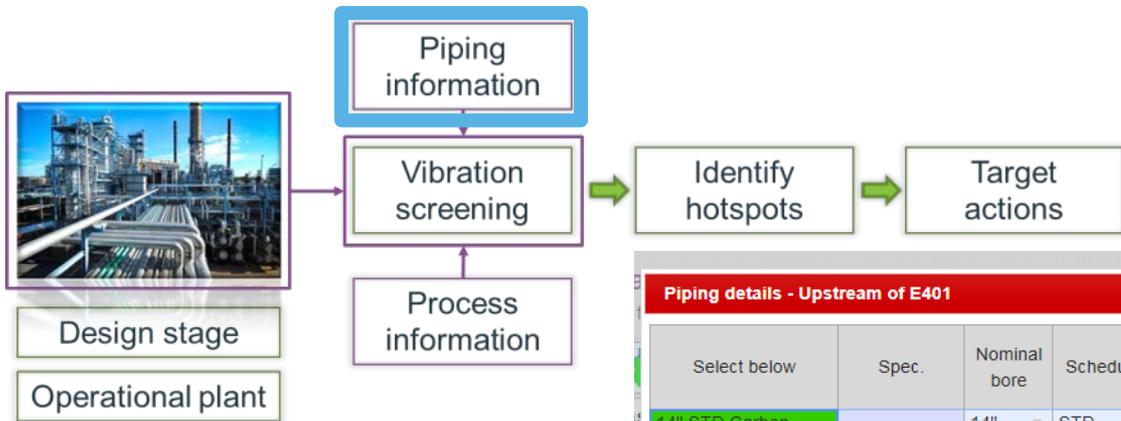
Free, web-based application that applies the EI standard to proactively identify piping vibration integrity threats



# Vibration screening approach



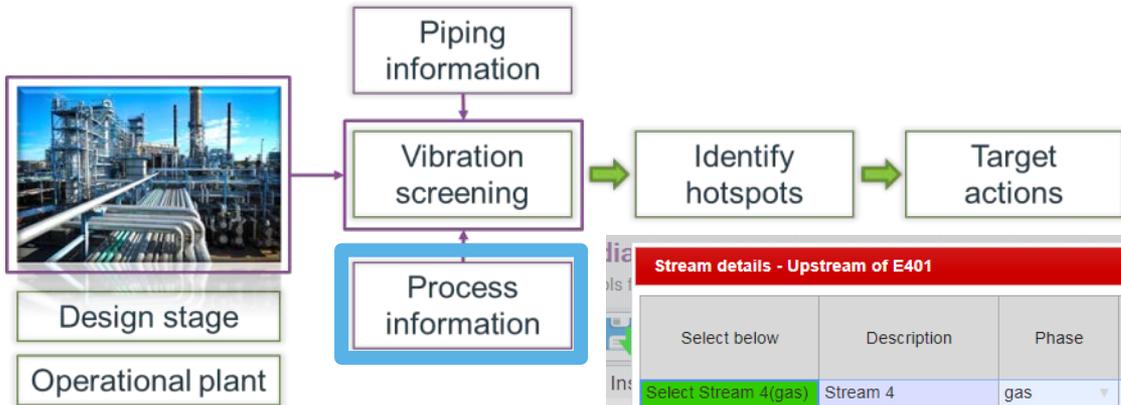
# Enter piping information



Piping details - Upstream of E401								
Select below	Spec.	Nominal bore	Schedule	Outside diameter [mm]	Wall thickness [mm]	Liner thickness [mm]	Material	Pipe Pressure Rating [bara]
14" STD Carbon Steel		14" ▾	STD ▾	355.6	9.525		Carbon Steel ▾	
8" 120 Carbon Steel		8" ▾	120 ▾	219.075	18.263		Carbon Steel ▾	
4" 120 Carbon Steel		4" ▾	120 ▾	114.3	11.125		Carbon Steel ▾	
6" STD Carbon Steel		6" ▾	STD ▾	168.275	7.112		Carbon Steel ▾	
20" STD Carbon Steel		20" ▾	STD ▾	508	9.525		Carbon Steel ▾	
12" STD Carbon Steel		12" ▾	STD ▾	323.85	9.525		Carbon Steel ▾	
10" STD Carbon Steel		10" ▾	STD ▾	273.05	9.271		Carbon Steel ▾	
							▾	
							▾	
							▾	
							▾	



# Enter stream information

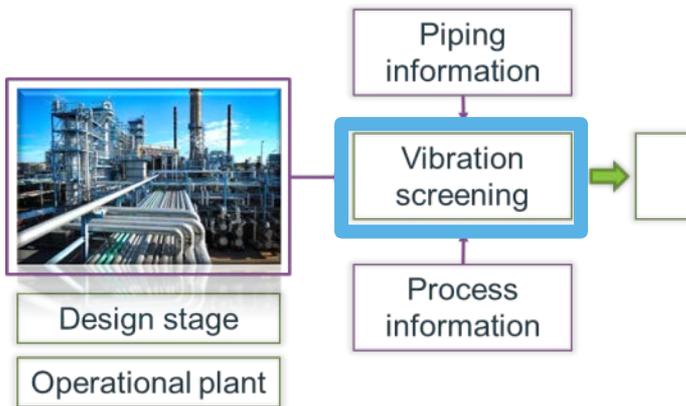


Stream details - Upstream of E401

Select below	Description	Phase	Mass flow rate [kg/h]	Temperature [°C]	Density [kg/m³]	Static pressure [Bara]	Dynamic viscosity [Pa.s]	Speed of sound [m/s]	Gamma (C <sub>p</sub> /C <sub>v</sub> ) [#]	Molecular weight [g/mol]
Select Stream 4(gas)	Stream 4	gas	59358	141.9	18	26	.00002	425.7984	1.22	23.22
Select Stream 5(gas)	Stream 5	gas	59358	30	26	24.5	.00001	375.6421	1.3	23.22
Select Stream 6(gas)	Stream 6	gas	53482	30	23	24.5	.00001	394.0547	1.34	21.75
Select Stream 7(gas)	Stream 7	gas	53482	136.7	62	88	.00002	456.4	1.33	21.75
Select Recycle low pressure(gas)	Recycle low pressure	gas	53482	141.9	18	26	.00002	425.7984	1.22	23.22
Select Relief high pressure(gas)	Relief high pressure	gas	53482	136.7	62	88	.00002	456.4	1.33	21.75
Select Relief low pressure(gas)	Relief low pressure	gas	53482	88	4	1	.00001	428.4	1.33	21.75
Select Stream 1 (original)(multiphase)	Stream 1 (original)	multiphase	461764	50	930	6.5	0	310.8077	1.01	28.09
Select Stream 2 (original)(gas)	Stream 2 (original)	gas	27180	50	5	6.5	.00001	389.2291	1.24	21.99
Select Stream 3 (original)(liquid)	Stream 3 (original)	liquid	303180	50	930	6.5	.3935	275.2810	1.08	38.29



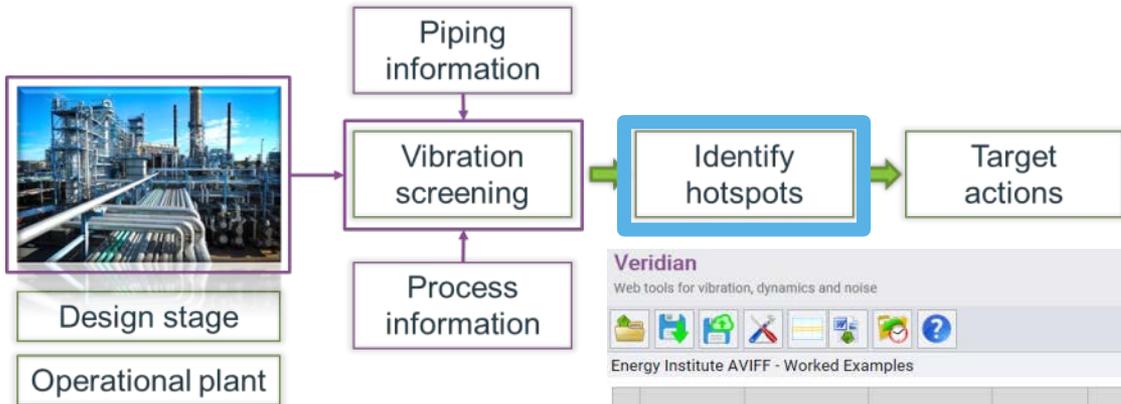
# Qualitative screening



Modules / Qualitative Assessment	
(FIT) Flow-induced turbulence (EI AVIFF Guidelines T2.2)	(fit)
Is the maximum value of kinetic energy ( $pv^2$ ) of the process fluid above 5000 kg/m s <sup>2</sup> ?	Yes <input checked="" type="checkbox"/>
Mechanical Excitation (EI AVIFF Guidelines T2.3)	(mex)
Is there any rotating or reciprocating machinery?	No <input checked="" type="checkbox"/>
Pulsation from reciprocating items (EI AVIFF Guidelines T2.4)	(rec)
Are there any positive displacement pumps or compressors?	No <input checked="" type="checkbox"/>
Pulsation from rotating stall (EI AVIFF Guidelines T2.5)	(rst)
Are there any centrifugal compressors which have the potential to operate under rotating stall conditions?	No <input checked="" type="checkbox"/>
Pulsation from corrugated pipes (EI Subsea AVIFF Guidelines E4.3)	(cor)
Does the system contain any rough bore flexibles?	No <input checked="" type="checkbox"/>
(AIV) High frequency acoustic excitation (EI AVIFF Guidelines T2.7)	(aiv)
Is choked flow possible, or are sonic flow velocities likely to be encountered? <b>only applies to pressure reducing systems, not the main line</b>	No <input checked="" type="checkbox"/>
Valve transients (EI AVIFF Guidelines T2.8)	(tra)
Are there any fast acting opening or closing valves?	No <input checked="" type="checkbox"/>
Thermowells (ASME PTC 19.3 TW - 2016)	(thw)
Are there any intrusive elements in the process stream?	No <input checked="" type="checkbox"/>
(SBC) Small bore connections (EI AVIFF Guidelines)	(sbc)
Are any of the main line LOF's $\geq 0.3$ ?	No <input checked="" type="checkbox"/>



# Qualitative screening



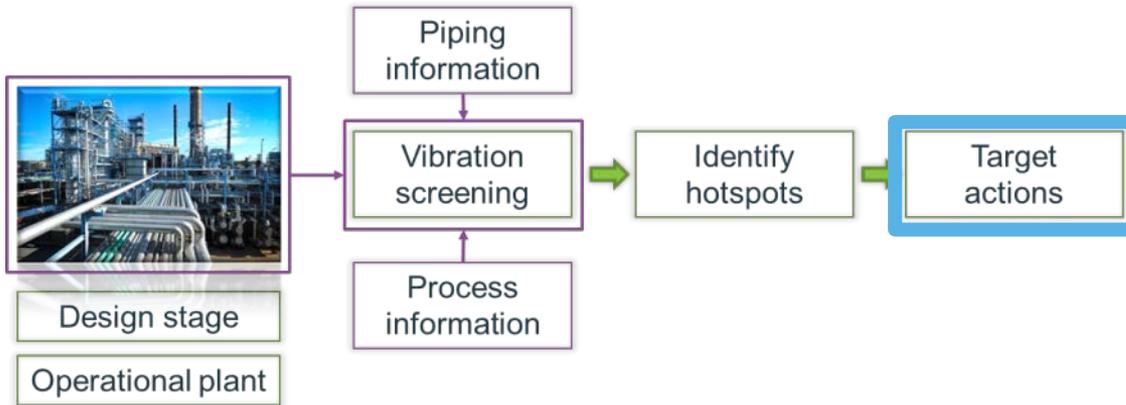
**Veridian**  
Web tools for vibration, dynamics and noise  
Signed in as [internal.demo](#) [Sign out](#)

Energy Institute AVIFF - Worked Examples

Record ID	P&ID	Line reference	Description	Notes	Pipe details	Stream	% of stream	Qualitative assessment (modules)	Flow-induced turbulence	Mechanical excitation	Pulsation Recip/PD	Pulsation from rotating stall	Pulsation from deadlegs	Pulsation from corrugations	Slugging flow	High frequency acoustic excitation	Valve transients	Cavitation and flashing	Thermowells	Small bore connections
1	Figure D-1	Stream 4	Upstream of E401		14" STD Carbon Steel	Stream 4 (gas)	100	v=10.3 m/s pv²= 1,909	0.01			0.00								
2	Figure D-1	Stream 5	Downstream of E401, upstream of		14" STD Carbon Steel	Stream 5 (gas)	100	v=7.1 m/s pv²= 1,321	0.01			0.00								
3	Figure D-1	Stream 6	Downstream of V402, upstream of		14" STD Carbon Steel	Stream 6 (gas)	100	v=7.3 m/s pv²= 1,213	0.01	0.40		0.00							0.29	
4	Figure D-1	Stream 7	Downstream of K402		8" 120 Carbon Steel	Stream 7 (gas)	100	v=9.2 m/s pv²= 5,197	0.02	0.40		1.00								0.66
5	Figure D-1	Recycle line (compressor)	From downstream of K402 back to		8" 120 Carbon Steel	Stream 7 (gas)	100	v=9.2 m/s pv²= 5,197	0.02	0.40		0.00			0.29					
6	Figure D-1	Recycle line (compressor)	From upstream of recycle valve to		6" STD Carbon Steel	Recycle low pressure(gas)	100	v=44.3 m/s pv²= 35,294	0.28			0.00			0.29					
7	Figure D-1	Relief line (upstream of PSV)	Downstream of K402 to upstream		4" 120 Carbon Steel	Relief high pressure(gas)	100	v=36.0 m/s pv²= 80,379	0.34	0.40		0.29							3.77	
8	Figure D-1	Relief line (downstream of PSV to flare)	Downstream of PSV to flare		6" STD Carbon Steel	Relief low pressure(gas)	100	v=199 m/s pv²= 1.59e5	0.88			1.00				1.48	1.77			
9	Figure D-3	Stream 1	From production		20" STD	Stream 1	100	v=9.3 m/s	0.02											



# Target actions



# Target actions



Veridian  
Web tools for vibration, dynamics and noise  
Signed in as [jordan.grose@woodgroup.com](mailto:jordan.grose@woodgroup.com) Sign out

System 2/System 2 - Electrostatic Treatment\_R00

Record ID	P&ID	Line reference	Description	Notes	Pipe details	Stream	% of stream	Qualitative assessment (modules)	Flow-induced turbulence	Valve transients	Cavitation and flashing	Small bore connections
1	0381-MI20-90DP-3190	14'-PL-A5D-19023-2H1	1st Stg. Electrostatic		14" CBI-ASD 10S Stainless Steel	Stream 1009 (Max Oil) (liquid)	50	v=2.2 m/s pv=3.662	0.15			
2	0381-MI20-90DP-3190	14'-PL-A5D-19023-2H1	1st Stg. Electrostatic		14" CBI-ASD 10S Stainless Steel	Stream 1009 (Max Oil) (liquid)	50	v=2.2 m/s pv=3.662	0.15			
3	0381-MI20-90DP-3190	14'-PL-A5D-19023-2H1	1st Stg. Electrostatic		14" CBI-ASD 10S Stainless Steel	Stream 1009 (Max Oil) (liquid)	100	v=4.3 m/s pv=14.648	1.38	0.10	0.00	0.74
4	0381-MI20-90DP-3190	14'-A5D-2RNX-19063	1st Stg. Electrostatic		14" CBI-ASD 10S Stainless Steel	Stream 1010 (Max Oil) (liquid)	100	v=3.2 m/s pv=8.173	0.77	0.60	1.00	0.66
5	0381-MI20-90DP-3190	14'-A5D-2RNX-19064	1st Stg. Electrostatic		14" CBI-ASD 10S Stainless Steel	Stream 1011 (Max Oil) (multiphase)	100	v=7.9 m/s pv=20.085	0.83	0.47	1.00	0.68
6	0381-MI20-90DP-3190	16'-PL-A5D-19024-2H1	1st Stg. Electrostatic		16" CBI-ASD 10S Stainless Steel	Stream 1012 (Max Oil) (multiphase)	100	v=6.1 m/s pv=12.098	0.49	0.14	1.00	0.70
7	0381-MI20-90DP-3192	16'-A5D-2RNX-19233	1st Stg. Electrostatic		16" CBI-ASD 10S Stainless Steel	Stream 1013 (Max Oil) (multiphase)	100	v=14.3 m/s pv=28.322	1.14			0.64
8	0381-MI20-90DP-3192	None	1st Stg. Electrostatic		18" CBI-ASD 10S Stainless Steel	Stream 1013 (Max Oil) (multiphase)	100	v=11.2 m/s pv=17.493	0.68			
9	0381-MI20-90DP-3190	None	1st Stg. Electrostatic		6" CBI-ASD 10S Stainless Steel	Stream 4502 (Max Oil) (liquid)	100	v=0.4 m/s pv=1.21	0.01			
10	0381-MI20-90DP-3190	3'-ASD-5RSX-19069	1st Stg. Electrostatic		3" CBI-ASD 10S Stainless Steel	Stream 4502 (Max Oil) (liquid)	100	v=1.3 m/s pv=1.748	0.08	1.00	0.00	



# When to perform a screening and why?

- New facility
  - FEED
  - Detailed design
  - Results in a better designed system
- Existing facility
  - If vibration risk is unknown
  - When facility requirements change (during management of change)
  - Increased throughput
  - When designing the upgrade of a facility
  - Enables owners to know where to focus their effort



# Vibration screening (VS) can fill the gap

**Detailed design**

Vibration screening

**Operations**



# Case study

- Work scope: two assessments
  1. FIV on all main-line, hydrocarbon process pipework
  2. AIV on flare system pipework
- Three different facility design cases (including 100% and 120% design)
- All main-line pipework assessed for:
  - Flow-induced turbulence
  - Flow-induced pulsation/vibration (FIV)
  - Mechanical
  - Machinery-generated pulsation (reciprocating compressors)
  - Fast acting valves – eg, flashing, cavitation



# FIV results and recommendations

## 66 required actions identified

- 2 **critical priority** actions – require immediate attention
- 6 **high priority** actions – closeout target date <3 month
- 58 **medium priority** action – closeout target date <6 month
- (+ 61 **low priority** actions – closeout target date <12 month)

## Specific actions required:

- 13 anti-vibration brace drawings for fabrication, installation and subsequent operator check measurements
- 11 engineering actions
- 6 engineering actions followed by subsequent operator check measurements
- 18 check measurements
- 18 locations recommended for detailed vibration measurement survey under representative flow conditions



# AIV results and recommendations

**Identified 65 risk areas** on flare piping and common 42” header; welded tee, side branch and pipe support connections

- 10 sliding shoe pipe supports on 42” header cleared, based on detailed FEA modeling
- 11 connections require visual inspection to confirm appropriate bracing has been installed
- 5 require valve diffuser performance – if better than assumed then can be removed from list
- 6 weldolets require bolted or welded 2–plane braces installed
- 3 fabricated tees with repads on 12” local header to be extended to full encirclement wraps
- 15 sliding shoe pipe supports on 42” header to be extended to full encirclement wraps
- 15 other tee connections with repads on 42” header to be extended to full encirclement wraps



# Conclusion

- **Vibration** is a real threat that **should be included in an effective integrity program**
- Tools enable asset owners to **ensure current standards (EI) are applied**
- **Vibration screening tools** are available that implement the current standards (EI) to **quickly identify where attention is needed**
- **Required data is most likely already compiled** for your existing RBI program
- **Vibration can be managed proactively**, and this **allows owners to prevent costly fatigue failures**



# Thank you

Michael Cyca

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Vibration dynamics and noise

Wood

[woodplc.com/vdn](http://woodplc.com/vdn)

